

Analysis of Highrise Building (G+15) with Vertical Irregularities Using ETABS

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ABSTRACT: Seismic forces can cause significant structural damage or destruction. Multi-story RC buildings have been subjected to the most dangerous earthquakes, as we all know. The existence of irregularity in RC constructions was discovered to be the primary cause of failure. The vertical irregularity of the building stands it apart from other structures. These structures are substantially more sensitive to earthquakes. For irregular buildings, 3D analytical models of highrise buildings were created in this work. The influence of numerous vertical irregularities on the building is studied using the structural analysis tool "ETABS." The seismic analysis will be performed in accordance with IS 1893-part-1:2016, seismic zone – IV, and soil type – medium soil in all cases.
KEYWORDS: Vertical irregularity, Irregular building, high impact of irregularity.

I. INTRODUCTION

At present time it is necessary to build multi-storied irregular structures due to shortage of space and non-accessibility of uniform ground conditions. During an earthquake, the structure's failure begins at the weakest areas.

These structures are referred to as irregular structures since they have this discontinuity. Urban infrastructure is full with irregular structures. Irregularities in a structure are key variables that reduce the seismic performance of any structure, as earthquake loads inject additional shear and twisting in irregular structures

As absolute regularity is an idealisation that rarely occurs in practice, it is recognised that existing buildings are usually irregular. Due to a lack of space and the inaccessibility of uniform ground conditions, it is currently required to construct multi-story irregular constructions.

Irregularities in a structure are very critical characteristics that severely reduce the seismic performance of any structure, as earthquake loads

add extra shear and twisting in irregular structures. Those abnormal structural alignments in an elevation or plan were usually identified as one of the key actions of the collapse caused by a previous seismic motion.

Although structural imperfections are a mix of plan and vertical irregularities, many seismic regulations distinguish between the two. Horizontal irregularity (plan irregularity) can be classified using the following criteria:

- ❖ Torsional irregularity
- ❖ Re-entrant corner
- ❖ Floor slabs having excessive cut-out and openings
- ❖ Out of plane offset in vertical element
- ❖ Non-parallel lateral force system

The vertical irregularity can be classified based on the following factors.

- ❖ Stiffness irregularity
- ❖ Mass irregularity
- ❖ Vertical geometric irregularity
- ❖ In plane discontinuity in vertical elements resisting lateral force
- ❖ Strength irregularity
- ❖ Floating or stub column
- ❖ Irregular modes of oscillation in two principal plan direction

The massive loss of high-rise and low-rise buildings in recent severe earthquakes demonstrates why such investigations are critical in emerging countries like India. As a result, the seismic behaviour of asymmetric building systems has become a hot area for research around the world. Many investigations into the elastic and inelastic seismic behaviour of asymmetric systems have been conducted in order to determine the origin of such structures' seismic vulnerability.

The ELF technique, on the other hand, is predicated on a number of assumptions. These assumptions hold true for regular structures, i.e., structures with uniform stiffness, strength, and mass distributions across their height. In real building constructions, there is an irregular distribution of these properties. As a result, it's critical to create criteria that would allow the ELF approach to be used in the study of irregular structures. "It is true that additional research is required to confirm these restrictions. However, there can be no unambiguous enforceable terms without such constraints."

In the current context, many buildings have irregular design and elevation arrangements. In the future, they may be subjected to disastrous earthquakes. As a result, it is vital to assess the performance of both new and old structures in terms of earthquake resistance.

II. OBJECTIVE

Objectives of the present study are as follows:

1. To describe the philosophy of structural behaviour.
2. To present various aspects of structural behaviour that alter with irregularity.
3. To investigate and analyse the high-rise structure using Response spectrum analysis.
4. To compare the results of the Parent model and other created models with irregularity combinations in Etabs.

III. LITERATURE REVIEW

[1] The seismic analysis of all eight regular and irregular RC structures was carried out in this study.

There are two sorts of vertical anomalies to consider: stiffness and setback.

The failure of a multistory building owing to seismic loading usually begins at the area where the building has a weakness. This flaw causes the building to deteriorate, eventually leading to structural collapse. The story displacement is higher in rigidity uneven structures than in regular structures. In severely irregular constructions, story drift is strongest for irregular storylines.

The overturning moment and story shear force of rigidity irregular constructions are slightly higher than those of regular buildings. The slope of the shear force curve increased moderately at the uneven story's. In stiffness irregular buildings, a drastic drop in the stiffness of the building has been seen at the uneven stories. These anomalies should

be avoided wherever possible, but if they must be included, they must be developed well.

[2]. The special moment-resisting frame is the primary LFRS intended for structures (SMRF). The constructions are typically cast-in-place reinforced concrete structures with monolithic beams supported by columns and monolithic slabs.

In the direction of the earthquake, all structures have three bays. The bay sizes are modified within practical bounds in order to investigate their impact on seismic response. Buildings of three various height categories, including 5-, 10-, and 20-story systems, are also evaluated. Normal-weight concrete with a 28-day cylinder strength of 5 KSI and A615 Grade 60 reinforcing is used for the beams and columns.

[3]. An analogous static approach was used to investigate the seismic response of regular and vertically uneven multi-story building frames in this paper. The paper's G+2, G+5, and G+11 story frames were examined with ETABS 16.1.0. (2016).

A total of nine models were examined, with zone 5 being utilised to assess the effects on building story displacement, story drift, and story shear. It contains a comparison of the results acquired from the examination of all of the building frames.

[4]. The following is the methodology that will be used to attain the objectives: -

1. Various Indian Design Codes for earthquake resistant analysis and design will be examined, as well as various code provisions for irregular structures.
2. A thorough investigation will be conducted into all aspects of a structure, including floating a column, types of imperfections in a structure, the effects of pounding on a structure, and the impacts of an earthquake on RC structures.
3. All general parameters of a building will be decided, such as frame a material, material constants, types, and intensities of a loading, and loading combinations.
4. The seismic coefficient approach will be used to perform the manual calculation for a base shear.
5. The modelling and analysis will be completed using a dependable programme (STAAD PRO). The required results will be reviewed and compared after assessing all of the selected models using selected materials.

[5]. In terms of cost and performance, steel-concrete composite structures outperform traditional RCC constructions. As a result,

imperfections must be considered while analysing composite constructions, and performance must be compared to RCC buildings.

The subject of this article is a ten-story RCC and composite building with various vertical imperfections. Individual models with irregularities at the bottom, middle, and top of the structure are modelled for study, with irregularities at the 2nd, 5th, and 9th floors. Each model has an irregularity at a different level of the structure. Irregularities are not allowed to be placed at the roof level, according to the code.

To investigate the impact of irregularities, Etabs was used to do a response spectrum analysis on the building model. The effects of various vertical irregularities on the RCC and composite constructions are compared and studied.

[6]. The goal of this work is to do a non-linear static pushover analysis of medium-height RC buildings and look at how structural behaviour varies when shear walls are taken into account. In this work, multi-story buildings (eight stories) located in zone III of medium soil sites were studied using the Indian code's Linear Static and Linear Dynamic methods and evaluated utilising pushover analysis as required in ATC-40 and FEMA-356. The Etabs analysis package is used for the analysis.

Three-dimensional frame elements are used to model columns and beams. Rigid diaphragms are used to model slabs. The joints

between the beam and the column are believed to be rigid. ETABS provides default hinge properties. Various construction components are modelled using software as explained.

On eight story building models on flat ground and sloping ground, three distinct assessments are carried out, as follows:

1. Equivalent Static Analysis
2. Response Spectrum Analysis
3. Pushover analysis

In this research, numerous models are constructed and tested in order to determine the parameters.

IV. METHODOLOGY

For the purpose of structural analysis. The ETABS software is used to model the building, and the Response spectrum analysis method is used to analyze the multi-story building. The seismic zone is V, and the soil type is Medium.

Vertical irregularity is added in building models, and a combination of it also added in the models. These forms of irregularities introduce different aspects for analysis in models.

In the models, we incorporate vertical irregularities at three levels

- Base
- Middle (7th story)
- Terrace,

Vertical irregularities are created by altering the model's parameters.

Table-1: Changes to be made to the parameters for vertical irregularity

| Types of irregularity | Changes | Parameter |
|---------------------------------|--|----------------------|
| Stiffness irregularity | Height of that floor | 4.5 m |
| Mass irregularity | SDL of that floor | 20 KN/m ² |
| Vertical geometric irregularity | Setback in building | after every 4 story |
| In-plane discontinuity | Displace the column of one side throughout from that floor | 200 mm |
| Stub column | column supported on beam on that floor | pin supported |

4.1 MODEL DESCRIPTION

4.1.1 data of parent model

Table-2: Model data in ETABS for parent model

| Description | Data values |
|---|---------------------|
| Material property | |
| Concrete grade | M30 |
| Steel grade | Fe500 |
| Building data | |
| Story | G+15 |
| Story height (m) | 3.2 (at all levels) |
| Beam size (mm) | 300 x 600 |
| Column size (mm) | 525 x 525 |
| Slab thickness (mm) | 150 |
| Soli type | II |
| Seismic zone | V |
| Wind speed (m/s) | 39 |
| Importance factor | 1.5 |
| Response reduction factor | 5 |
| Loading data | |
| Floor finish (SDL) (KN/m ²) | 1.5 |
| Live load at typical floor (KN/m ²) | 2 |
| Roof live load (KN/m ²) | 1.5 |
| Roof dead load (SDL) (KN/m ²) | 2.5 |
| Type of support (KN/m ²) | Fix |

Table-3: Story displacement of parent model in EQx dir.

| STORY | ELEVATION (m) | X-Dir. (mm) | Y - Dir. (mm) |
|-----------------------|---------------|-------------|---------------|
| TERRACE | 54.4 | 104.741 | 0 |
| 14 th F.S. | 51.2 | 103.05 | 0 |
| 13 th F.S. | 48 | 100.36 | 0 |
| 12 th F.S. | 44.8 | 96.702 | 0 |
| 11 th F.S. | 41.6 | 92.181 | 0 |
| 10 th F.S. | 38.4 | 86.908 | 0 |
| 9 th F.S. | 35.2 | 80.988 | 0 |
| 8 th F.S. | 32 | 74.521 | 0 |
| 7 th F.S. | 28.8 | 67.599 | 0 |
| 6 th F.S. | 25.6 | 60.307 | 0 |
| 5 th F.S. | 22.4 | 52.723 | 0 |

| | | | |
|----------------------|------|--------|-------|
| 4 th F.S. | 19.2 | 44.917 | 0 |
| 3 rd F.S. | 16 | 36.951 | 0 |
| 2 nd F.S. | 12.8 | 28.881 | 0 |
| 1 st F.S. | 9.6 | 20.76 | 0 |
| GF SLAB | 6.4 | 12.668 | 0 |
| PLT. LVL. | 3.2 | 4.911 | 0.002 |
| Base | 0 | 0 | 0 |

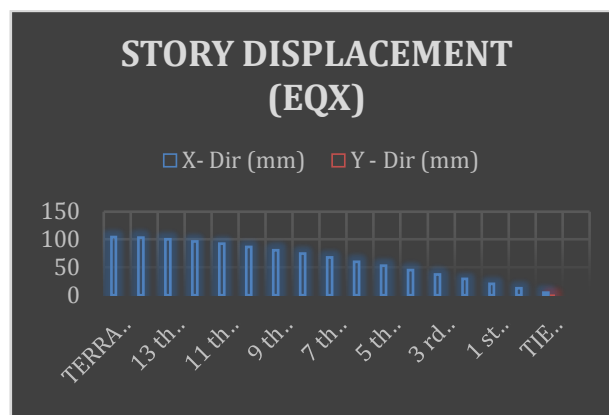


Fig-1: Story displacement of parent model in EQxdir.

Table-4: Story displacement of parent model in EQy dir.

| STORY | ELEVATION (m) | X- Dir. (mm) | Y - Dir. (mm) |
|-----------------------|---------------|--------------|---------------|
| TERRACE | 54.4 | 0 | 104.741 |
| 14 th F.S. | 51.2 | 0 | 103.05 |
| 13 th F.S. | 48 | 0 | 100.36 |
| 12 th F.S. | 44.8 | 0 | 96.702 |
| 11 th F.S. | 41.6 | 0 | 92.181 |
| 10 th F.S. | 38.4 | 0 | 86.908 |
| 9 th F.S. | 35.2 | 0 | 80.988 |
| 8 th F.S. | 32 | 0 | 74.521 |
| 7 th F.S. | 28.8 | 0 | 67.599 |
| 6 th F.S. | 25.6 | 0 | 60.307 |
| 5 th F.S. | 22.4 | 0 | 52.723 |

| | | | |
|----------------------|------|-------|--------|
| 4 th F.S. | 19.2 | 0 | 44.917 |
| 3 rd F.S. | 16 | 0 | 36.951 |
| 2 nd F.S. | 12.8 | 0 | 28.881 |
| 1 st F.S. | 9.6 | 0 | 20.76 |
| GF SLAB | 6.4 | 0 | 12.668 |
| PLT. LVL. | 3.2 | 0.002 | 4.911 |
| Base | 0 | 0 | 0 |

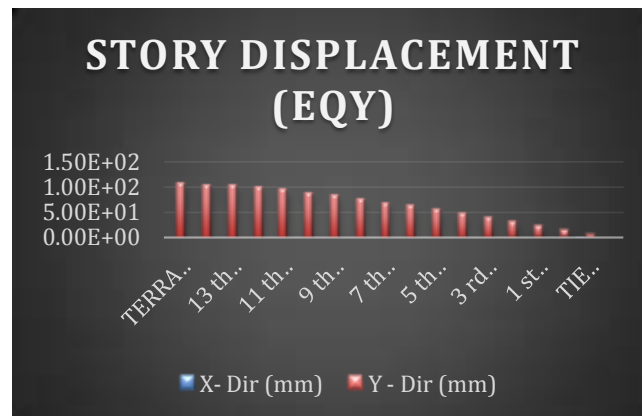


Fig-2: Story displacement of parent model in EQy dir.

Table-5: Story drift of parent model in EQx dir.

| STORY | ELEVATION (m) | X-Dir. (mm) | Y - Dir. (mm) |
|-----------------------|---------------|-------------|---------------|
| TERRACE | 54.4 | 0.000528 | 0 |
| 14 th F.S. | 51.2 | 0.000841 | 0 |
| 13 th F.S. | 48 | 0.001143 | 0 |
| 12 th F.S. | 44.8 | 0.001413 | 0 |
| 11 th F.S. | 41.6 | 0.001648 | 0 |
| 10 th F.S. | 38.4 | 0.00185 | 0 |
| 9 th F.S. | 35.2 | 0.002021 | 0 |
| 8 th F.S. | 32 | 0.002163 | 0 |
| 7 th F.S. | 28.8 | 0.002279 | 0 |
| 6 th F.S. | 25.6 | 0.00237 | 0 |
| 5 th F.S. | 22.4 | 0.00244 | 0 |

| | | | |
|----------------------|------|----------|-----------------------|
| 4 th F.S. | 19.2 | 0.002489 | 0 |
| 3 rd F.S. | 16 | 0.002522 | 0 |
| 2 nd F.S. | 12.8 | 0.002538 | 0 |
| 1 st F.S. | 9.6 | 0.002529 | 0 |
| GF SLAB | 6.4 | 0.002444 | 1.00*10 ⁰⁶ |
| PLT. LVL. | 3.2 | 0.001535 | 1.00*10 ⁰⁶ |
| Base | 0 | 0 | 0 |

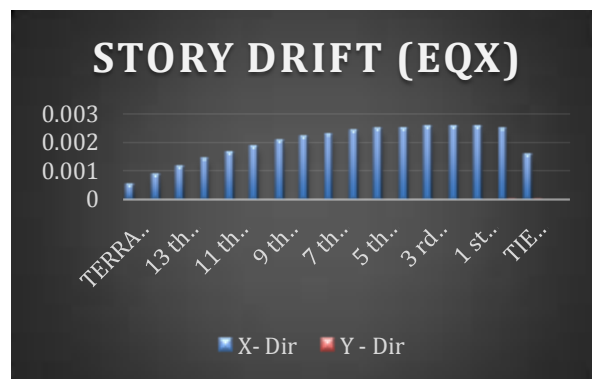


Fig-3: Story drift of parent model in EQx dir.

Table-6: Story drift of parent model in EQy dir.

| STORY | ELEVATION (m) | X- Dir. (mm) | Y - Dir. (mm) |
|-----------------------|---------------|--------------|---------------|
| TERRACE | 54.4 | 0 | 0.000528 |
| 14 th F.S. | 51.2 | 0 | 0.000841 |
| 13 th F.S. | 48 | 0 | 0.001143 |
| 12 th F.S. | 44.8 | 0 | 0.001413 |
| 11 th F.S. | 41.6 | 0 | 0.001648 |
| 10 th F.S. | 38.4 | 0 | 0.00185 |
| 9 th F.S. | 35.2 | 0 | 0.002021 |
| 8 th F.S. | 32 | 0 | 0.002163 |
| 7 th F.S. | 28.8 | 0 | 0.002279 |
| 6 th F.S. | 25.6 | 0 | 0.00237 |
| 5 th F.S. | 22.4 | 0 | 0.00244 |
| 4 th F.S. | 19.2 | 0 | 0.002489 |

| | | | |
|----------------------|------|-----------------------|----------|
| 3 rd F.S. | 16 | 0 | 0.002522 |
| 2 nd F.S. | 12.8 | 0 | 0.002538 |
| 1 st F.S. | 9.6 | 0 | 0.002529 |
| GF SLAB | 6.4 | 1.00*10 ⁰⁶ | 0.002444 |
| PLT. LVL. | 3.2 | 1.00*10 ⁰⁶ | 0.001535 |
| Base | 0 | 0 | 0 |

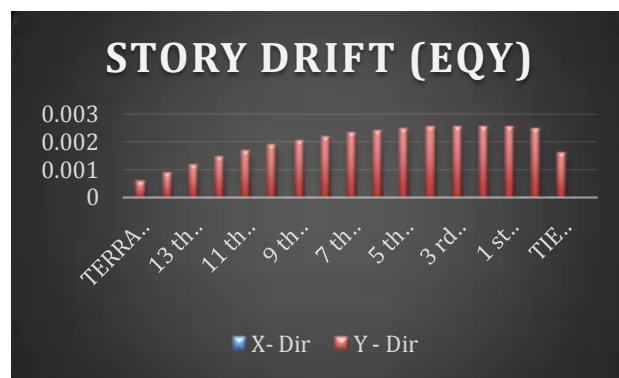


Fig-4: Story drift of parent model in EQy dir.

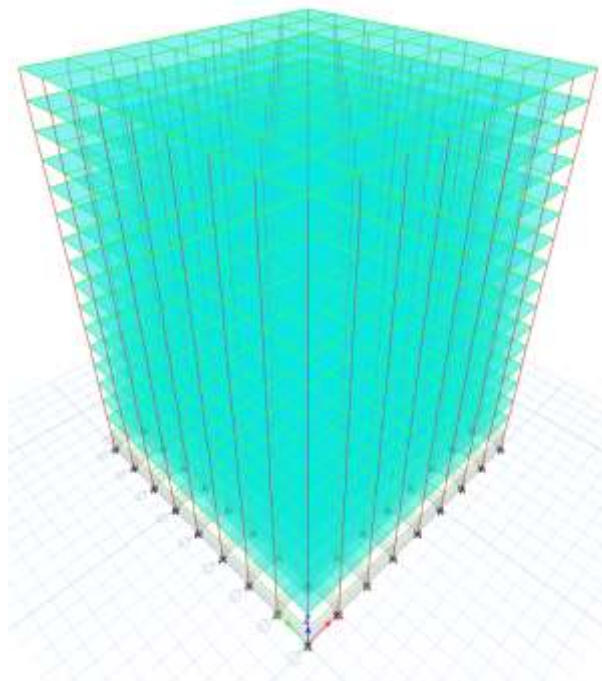


Fig-5: 3-D view of parent model

4.1.2 List and description of models which is prepared

Case 1 - Model having Stiffness irregularity

- Comb. 1 - Height of ground floor is 4.5 m
- Comb. 2 - Height of 7th floor is 4.5 m
- Comb. 3 - Height of terrace floor is 4.5 m
- Comb. 4 - Height of ground & 7th floor is 4.5 m
- Comb. 5 - Height of ground & terrace floor is 4.5 m
- Comb. 6 - Height of 7th & terrace floor is 4.5 m
- Comb. 7 - Height of ground, 7th & terrace floor is 4.5 m

Case 2 - Model having Mass irregularity

- Comb. 8 - Load on ground floor is 20 KN/m²
- Comb. 9 - Load on 7th floor is 20 KN/m²
- Comb. 10 - Load on terrace floor is 20 KN/m²
- Comb. 11 - Load on ground & 7th floor is 20 KN/m²
- Comb. 12 - Load on ground & terrace floor is 20 KN/m²
- Comb. 13 - Load on 7th & terrace floor is 20 KN/m²
- Comb. 14 - Load on ground, 7th & terrace floor is 20 KN/m²

Case 3 - Model having Vertical geometrical irregularity

- Comb. 15 - a) Setback in Y-dir. after every 4 story from G.F.
- Comb. 16 - a) Setback in X & Y-dir. after every 4 story from G.F.
- Comb. 17 - a) Setback in Y-dir. after every 4 story from 7th floor
- Comb. 18 - a) Setback in X & Y-dir. after every 4 story from 7th floor
- Comb. 19 - b) Setback in Y-dir. after every 4 story from G.F. on both side
- Comb. 20 - b) Setback in X & Y-dir. after every 4 story from G.F. on both side
- Comb. 21 - b) Setback in Y-dir. after every 4 story from 7th floor on both side
- Comb. 22 - b) Setback in X & Y-dir. after every 4 story from 7th floor on both side
- Comb. 23 - c) Setback in Y-dir. from 1ST F. on both side
- Comb. 24 - c) Setback in X & Y-dir. from 1ST F. on both side

Case 4 - Model having In-plane discontinuity

- Comb. 25 - Shift the column of one side to 200 mm from 7th floor
- Comb. 26 - Shift the column of one side to 200 mm from terrace floor
- Comb. 27 - Shift the column of one side to 200 mm from 7th & terrace floor

Case 5 - Model having Stub column

- Comb. 28 - Stub column from G.F.
- Comb. 29 - Stub column from 7th floor
- Comb. 30 - Stub column from G.F. & 7th floor

Case 6 - Model having Stiffness & Mass irregularity [Description + (Height of floor – 4.5m)]

- Comb. 33 - Load on ground floor is 20 KN/m²
- Comb. 34 - Load on 7th floor is 20 KN/m²
- Comb. 35 - Load on terrace floor is 20 KN/m²
- Comb. 36 - Load on ground & 7th floor is 20 KN/m²
- Comb. 37 - Load on ground & terrace floor is 20 KN/m²
- Comb. 38 - Load on 7th & terrace floor is 20 KN/m²
- Comb. 39 - Load on ground, 7th & terrace floor is 20 KN/m²

Case 7 - Model having Stiffness & Vertical geometric irregularity [Description + (Height of floor – 4.5m)]

- Comb. 40 - a) Setback in Y-dir. after every 4 story from G.F.
- Comb. 41 - a) Setback in X & Y-dir. after every 4 story from G.F.
- Comb. 42 - a) Setback in Y-dir. after every 4 story from 7th floor
- Comb. 43 - a) Setback in X & Y-dir. after every 4 story from 7th floor
- Comb. 44 - b) Setback in Y-dir. after every 4 story from G.F. on both side
- Comb. 45 - b) Setback in X & Y-dir. after every 4 story from G.F. on both side
- Comb. 46 - b) Setback in Y-dir. after every 4 story from 7th floor on both side
- Comb. 47 - b) Setback in X & Y-dir. after every 4 story from 7th floor on both side
- Comb. 48 - c) Setback in Y-dir. from 1ST F. on both side
- Comb. 49 - c) Setback in X & Y-dir. from 1ST F. on both side

Case 8 - Model having Stiffness & In-plane discontinuity irregularity [Description + (Height of floor – 4.5m)]

- Comb. 50 - Shift the column of one side to 200 mm from 7th floor
- Comb. 51 - Shift the column of one side to 200 mm from terrace floor
- Comb. 52 - Shift the column of one side to 200 mm from 7th & terrace floor

Case 9 - Model having Stiffness & stub column irregularity [Description + (Height of floor – 4.5m)]

- Comb. 53 - Stub column from G.F.
- Comb. 54 - Stub column from 7th floor
- Comb. 55 - Stub column from G.F. & 7th floor

Case 10 - Model having Mass & Vertical geometry irregularity [Description + (Mass on that floor – 20KN/m²)]

- Comb. 56 - a) Setback in Y-dir. after every 4 story from G.F.
- Comb. 57 - a) Setback in X & Y-dir. after every 4 story from G.F.
- Comb. 58 - a) Setback in Y-dir. after every 4 story from 7th floor
- Comb. 59 - a) Setback in X & Y-dir. after every 4 story from 7th floor
- Comb. 60 - b) Setback in Y-dir. after every 4 story from G.F. on both side
- Comb. 61 - b) Setback in X & Y-dir. after every 4 story from G.F. on both side
- Comb. 62 - b) Setback in Y-dir. after every 4 story from 7th floor on both side
- Comb. 63 - b) Setback in X & Y-dir. after every 4 story from 7th floor on both side
- Comb. 64 - c) Setback in Y-dir. from 1ST F. on both side
- Comb. 65 - c) Setback in X & Y-dir. from 1ST F. on both side

Case 11 - Model having Mass & In-plane discontinuity irregularity [Description + (Mass on that floor – 20KN/m²)]

- Comb. 66 - Shift the column of one side to 200 mm from 7th floor
- Comb. 67 - Shift the column of one side to 200 mm from terrace floor
- Comb. 68 - Shift the column of one side to 200 mm from 7th & terrace floor

Case 12 - Model having Mass & Stub column irregularity [Description + (Mass on that floor – 20KN/m²)]

- Comb. 69 - Stub column from G.F.
- Comb. 70 - Stub column from 7th floor
- Comb. 71 - Stub column from G.F. & 7th floor

Case 13 – Model having Vertical geometric & In-plane discontinuity irregularity [Description + (Shift the column of one side 200 mm)]

- Comb. 72 - a) Setback in Y-dir. after every 4 story from G.F.
- Comb. 73 - a) Setback in X & Y-dir. after every 4 story from G.F.

Comb. 74 - a) Setback in Y-dir. after every 4 story from 7th floor

Comb. 75 - a) Setback in X & Y-dir. after every 4 story from 7th floor

Comb. 76 - b) Setback in Y-dir. after every 4 story from G.F. on both side

Comb. 77 - b) Setback in X & Y-dir. after every 4 story from G.F. on both side

Comb. 78 - b) Setback in Y-dir. after every 4 story from 7th floor on both side

Comb. 79 - b) Setback in X & Y-dir. after every 4 story from 7th floor on both side

Comb. 80 - c) Setback in Y-dir. from 1ST F. on both side

Comb. 81 - c) Setback in X & Y-dir. from 1ST F. on both side

Case 14 - Model having Vertical geometric & Stub column irregularity [Description + (Stub column from that floor)]

Comb. 82 - a) Setback in Y-dir. after every 4 story from G.F.

Comb. 83 - a) Setback in X & Y-dir. after every 4 story from G.F.

Comb. 84 - a) Setback in Y-dir. after every 4 story from 7th floor

Comb. 85 - a) Setback in X & Y-dir. after every 4 story from 7th floor

Comb. 86 - b) Setback in Y-dir. after every 4 story from G.F. on both side

Comb. 87 - b) Setback in X & Y-dir. after every 4 story from G.F. on both side

Comb. 88 - b) Setback in Y-dir. after every 4 story from 7th floor on both side

Comb. 89 - b) Setback in X & Y-dir. after every 4 story from 7th floor on both side

Comb. 90 - c) Setback in Y-dir. from 1ST F. on both side

Comb. 91 - c) Setback in X & Y-dir. from 1ST F. on both side

4.1.3 Following load combinations are used in models

- DL + LL
- DL ± EQ_{x/y}
- DL + LL ± EQ_{x/y}
- 1.5DL
- 1.5(DL + LL)
- 1.2(DL + LL ± W_{x/y})
- 1.5(DL ± W_{x/y})
- 0.9DL ± 1.5W_{x/y}
- 1.2(DL + LL ± EQ_{x/y})
- 1.5(DL ± EQ_{x/y})
- 0.9DL ± 1.5EQ_{x/y}
- 1.2(DL + LL + RS_{x/y})
- 1.5(DL + RS_{x/y})
- 0.9DL + 1.5RS_{x/y}

V. RESULTS

All the indicating values are the Maximum value obtained from the analysis

Case 1 - Model having Stiffness irregularity

Table 7: Maximum parameters for case 1

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|--------|------|-------------------|------------------|
| Pa.Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 1 | EQx | 112.095176 | 0.003465 |
| | EQy | 112.095176 | 0.003465 |
| comb 2 | EQx | 111.750503 | 0.003145 |
| | EQy | 111.750503 | 0.003145 |
| comb 3 | EQx | 105.284182 | 0.002502 |
| | EQy | 105.284182 | 0.002502 |
| comb 4 | EQx | 118.903488 | 0.003417 |
| | EQy | 118.903488 | 0.003417 |
| comb 5 | EQx | 112.535175 | 0.003416 |
| | EQy | 112.535175 | 0.003416 |
| comb 6 | EQx | 112.228104 | 0.003109 |
| | EQy | 112.228104 | 0.003109 |
| comb 7 | EQx | 119.290022 | 0.003371 |
| | EQy | 119.290022 | 0.003371 |

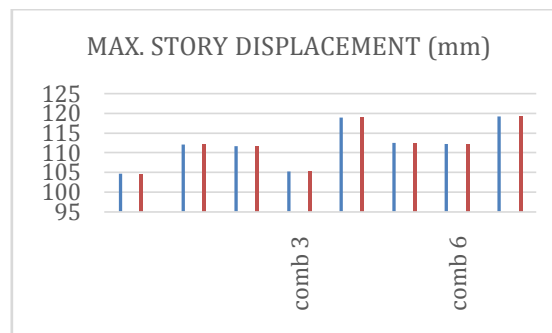


Fig-6: Maximum story displacement for case 1

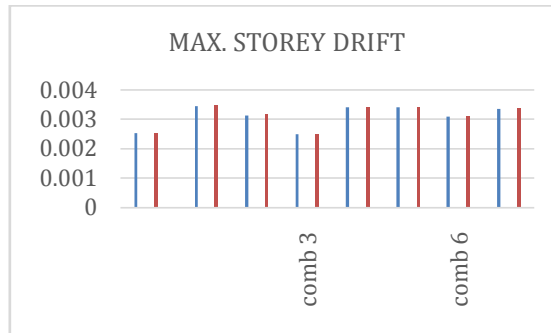


Fig-7: Maximum story displacement for case 1

Case 2 - Model having Mass irregularity

Table 8: Maximum parameters for case 2

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa.Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 8 | EQx | 104.843931 | 0.002538 |
| | EQy | 104.843931 | 0.002538 |
| comb 9 | EQx | 105.387414 | 0.002562 |
| | EQy | 105.387414 | 0.002562 |
| comb 10 | EQx | 105.698935 | 0.002561 |
| | EQy | 105.698935 | 0.002561 |
| comb 11 | EQx | 105.492523 | 0.002563 |
| | EQy | 105.492523 | 0.002563 |
| comb 12 | EQx | 105.803959 | 0.002562 |
| | EQy | 105.803959 | 0.002562 |
| comb 13 | EQx | 106.357609 | 0.002586 |
| | EQy | 106.357609 | 0.002586 |
| comb 14 | EQx | 106.464429 | 0.002587 |
| | EQy | 106.464429 | 0.002587 |

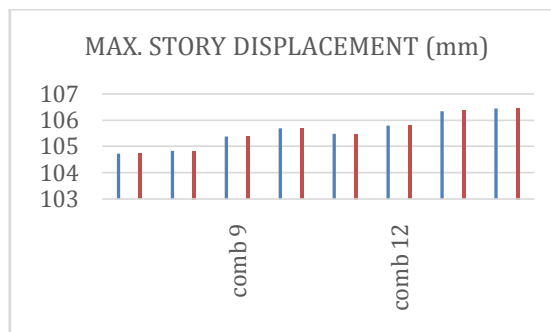


Fig-8: Maximum story displacement for case 2

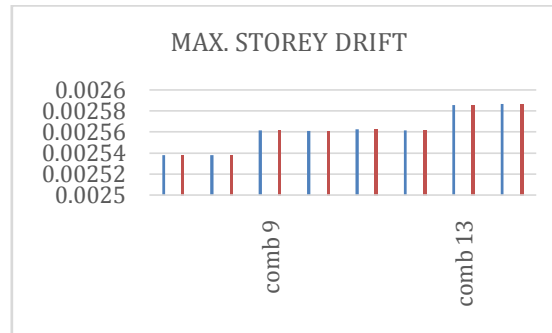


Fig-9: Maximum story displacement for case 2

Case 3 - Model having Vertical geometrical irregularity

Table 9: Maximum parameters for case 3

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 15 | EQx | 113.396709 | 0.002761 |
| | EQy | 94.994199 | 0.002189 |
| comb 16 | EQx | 105.504471 | 0.002448 |
| | EQy | 105.504471 | 0.002448 |
| comb 17 | EQx | 112.617525 | 0.00275 |
| | EQy | 96.697897 | 0.002284 |
| comb 18 | EQx | 104.465741 | 0.00248 |
| | EQy | 104.465741 | 0.00248 |
| comb 19 | EQx | 81.28044 | 0.001897 |
| | EQy | 84.477763 | 0.001944 |
| comb 20 | EQx | 76.890193 | 0.001925 |
| | EQy | 76.890193 | 0.001925 |
| comb 21 | EQx | 89.346767 | 0.002046 |
| | EQy | 88.223122 | 0.002036 |
| comb 22 | EQx | 79.664568 | 0.001755 |
| | EQy | 79.664568 | 0.001755 |
| comb 23 | EQx | 101.222975 | 0.002516 |
| | EQy | 105.182037 | 0.002609 |
| comb 24 | EQx | 103.277224 | 0.002623 |
| | EQy | 103.277224 | 0.002623 |

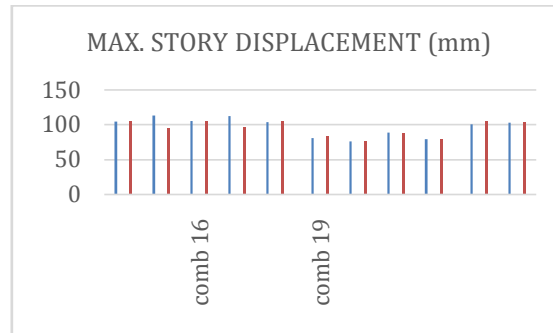


Fig-10: Maximum story displacement for case 3

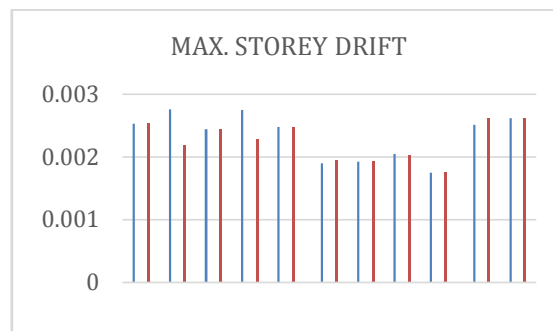


Fig-11: Maximum story displacement for case 3

Case 4 - Model having In-plane discontinuity

Table 10: Maximum parameters for case 4

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 25 | EQx | 105.412258 | 0.002543 |
| | EQy | 105.390577 | 0.002555 |
| comb 26 | EQx | 104.815743 | 0.002539 |
| | EQy | 104.983171 | 0.002542 |
| comb 27 | EQx | 105.487411 | 0.002544 |
| | EQy | 105.639341 | 0.00256 |

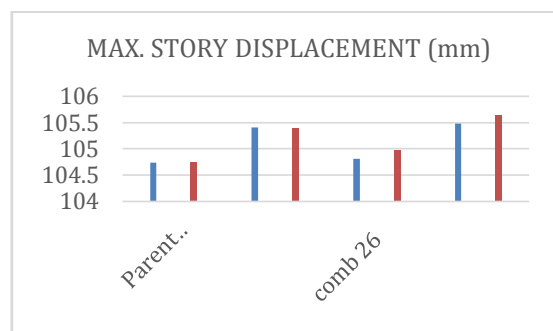


Fig-12: Maximum story displacement for case 4

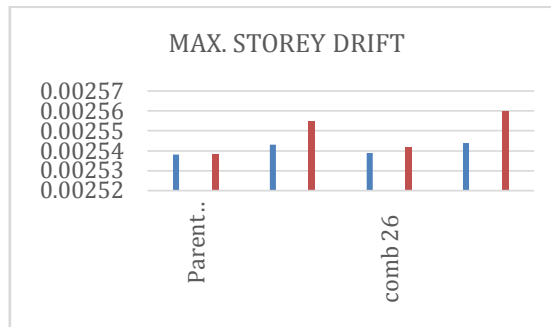


Fig-13: Maximum story displacement for case 4

Case 5 - Model having Stub column

Table 11: Maximum parameters for case 5

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 28 | EQx | 106.837335 | 0.002793 |
| | EQy | 108.067914 | 0.00275 |
| comb 29 | EQx | 106.647064 | 0.002562 |
| | EQy | 106.220592 | 0.002535 |
| comb 30 | EQx | 108.758624 | 0.002793 |
| | EQy | 109.026577 | 0.002748 |

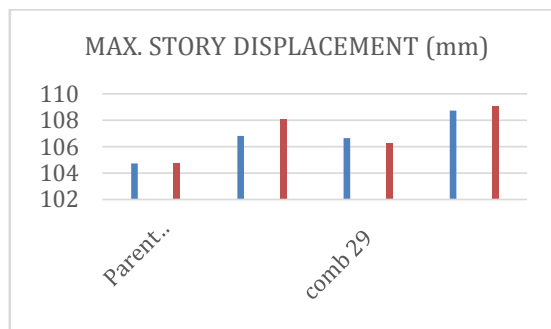


Fig-14: Maximum story displacement for case 5

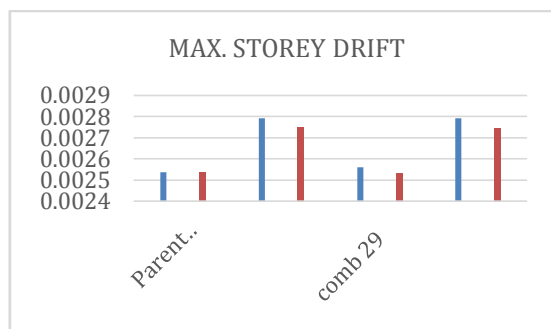


Fig-15: Maximum story displacement for case 5

Case 6 - Model having Stiffness & Mass irregularity

Table 12: Maximum parameters for case 6

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 33 | EQx | 112.347485 | 0.003502 |
| | EQy | 112.347485 | 0.003502 |
| comb 34 | EQx | 112.531127 | 0.00318 |
| | EQy | 112.531127 | 0.00318 |
| comb 35 | EQx | 106.262012 | 0.002525 |
| | EQy | 106.262012 | 0.002525 |
| comb 36 | EQx | 120.096224 | 0.003498 |
| | EQy | 120.096224 | 0.003498 |
| comb 37 | EQx | 113.911409 | 0.003495 |
| | EQy | 113.911409 | 0.003495 |
| comb 38 | EQx | 114.128711 | 0.003183 |
| | EQy | 114.128711 | 0.003183 |
| comb 39 | EQx | 121.74362 | 0.003493 |
| | EQy | 121.74362 | 0.003493 |

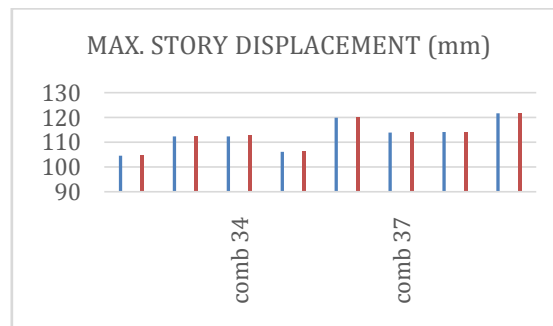


Fig-16: Maximum story displacement for case 6

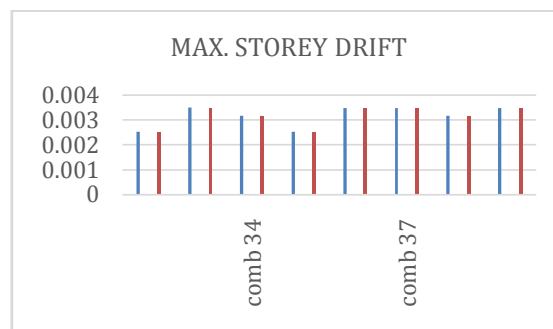


Fig-17: Maximum story displacement for case 6

Case 7 - Model having Stiffness & Vertical geometric irregularity

Table 13: Maximum parameters for case 7

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 40 | EQx | 121.434722 | 0.003802 |
| | EQy | 100.715104 | 0.002803 |
| comb 41 | EQx | 111.578736 | 0.003087 |
| | EQy | 111.578736 | 0.003087 |
| comb 42 | EQx | 120.218944 | 0.003397 |
| | EQy | 102.781568 | 0.002761 |
| comb 43 | EQx | 111.092227 | 0.002989 |
| | EQy | 111.092227 | 0.002989 |
| comb 44 | EQx | 85.389219 | 0.002149 |
| | EQy | 88.251899 | 0.002109 |
| comb 45 | EQx | 79.031405 | 0.001868 |
| | EQy | 79.031405 | 0.001868 |
| comb 46 | EQx | 94.689888 | 0.002402 |
| | EQy | 93.346766 | 0.00236 |
| comb 47 | EQx | 83.768879 | 0.001882 |
| | EQy | 83.768879 | 0.001882 |
| comb 48 | EQx | 106.496056 | 0.002692 |
| | EQy | 110.293044 | 0.002634 |
| comb 49 | EQx | 106.929616 | 0.002593 |
| | EQy | 106.929616 | 0.002593 |



Fig-18: Maximum story displacement for case 7

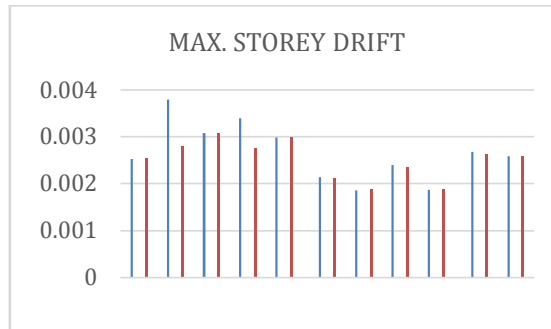


Fig-19: Maximum story displacement for case 7

Case 8 - Model having Stiffness & In-plane discontinuity irregularity

Table 14: Maximum parameters for case 8

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 50 | EQx | 112.608803 | 0.003194 |
| | EQy | 112.431435 | 0.003157 |
| comb 51 | EQx | 105.370439 | 0.002503 |
| | EQy | 105.545503 | 0.002506 |
| comb 52 | EQx | 113.18822 | 0.00316 |
| | EQy | 113.182111 | 0.003127 |

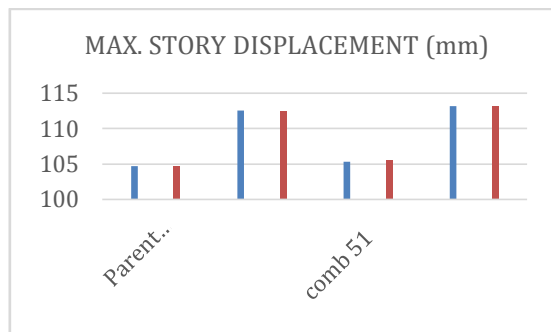


Fig-20: Maximum story displacement for case 8

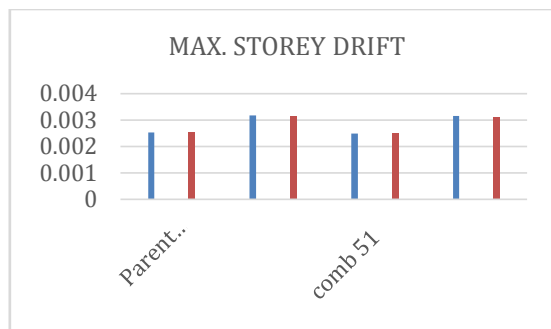


Fig-20: Maximum story displacement for case 8

Case 9 - Model having Stiffness & stub column irregularity

Table 15: Maximum parameters for case 9

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 53 | EQx | 115.490466 | 0.003972 |
| | EQy | 116.545723 | 0.003928 |
| comb 54 | EQx | 114.721575 | 0.003558 |
| | EQy | 113.984025 | 0.003435 |
| comb 55 | EQx | 125.176998 | 0.003915 |
| | EQy | 124.986428 | 0.003869 |

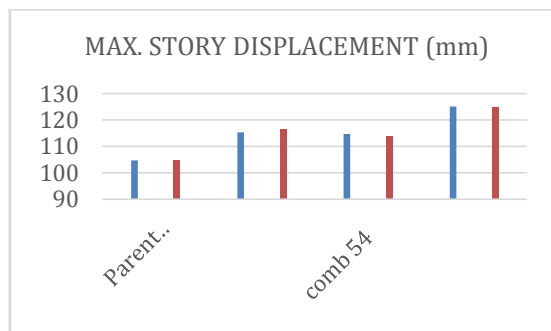


Fig-21: Maximum story displacement for case 9

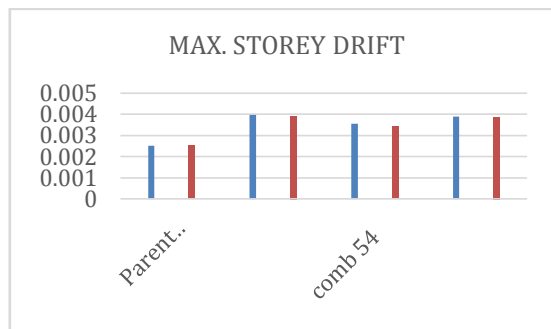


Fig-22: Maximum storey drift for case 9

Case 10 - Model having Mass & Vertical geometry irregularity

Table 16: Maximum parameters for case 10

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 56 | EQx | 113.750857 | 0.002785 |
| | EQy | 95.264119 | 0.00219 |
| comb 57 | EQx | 105.788802 | 0.002449 |
| | EQy | 105.788802 | 0.002449 |
| comb 58 | EQx | 113.295315 | 0.002776 |

| | | | |
|---------|-----|------------|----------|
| | EQy | 97.267703 | 0.002306 |
| comb 59 | EQx | 105.064781 | 0.002503 |
| | EQy | 105.064781 | 0.002503 |
| comb 60 | EQx | 81.48852 | 0.001897 |
| | EQy | 84.677928 | 0.001944 |
| comb 61 | EQx | 77.03725 | 0.001925 |
| | EQy | 77.03725 | 0.001925 |
| comb 62 | EQx | 89.855317 | 0.002066 |
| | EQy | 88.715048 | 0.002055 |
| comb 63 | EQx | 80.076765 | 0.001772 |
| | EQy | 80.076765 | 0.001772 |
| comb 64 | EQx | 101.302725 | 0.002516 |
| | EQy | 105.258702 | 0.002609 |
| comb 65 | EQx | 103.336925 | 0.002623 |
| | EQy | 103.336925 | 0.002623 |

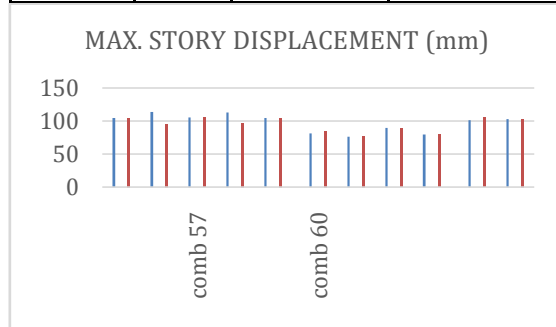


Fig-23: Maximum story displacement for case 10

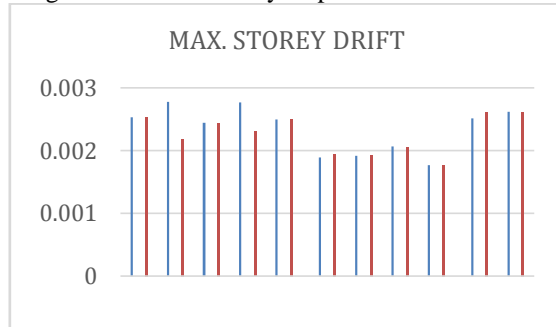


Fig-24: Maximum story displacement for case 10

Case 11 - Model having Mass & In-plane discontinuity irregularity

Table 17: Maximum parameters for case 11

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 66 | EQx | 106.066951 | 0.002567 |
| | EQy | 106.048987 | 0.00258 |
| comb 67 | EQx | 105.779638 | 0.002562 |
| | EQy | 105.954204 | 0.002566 |
| comb 68 | EQx | 107.13361 | 0.002593 |

| | | | |
|--|-----|------------|----------|
| | EQy | 107.298292 | 0.002609 |
|--|-----|------------|----------|

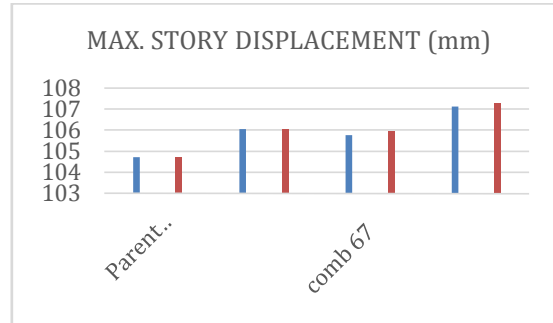


Fig-25: Maximum story displacement for case 11

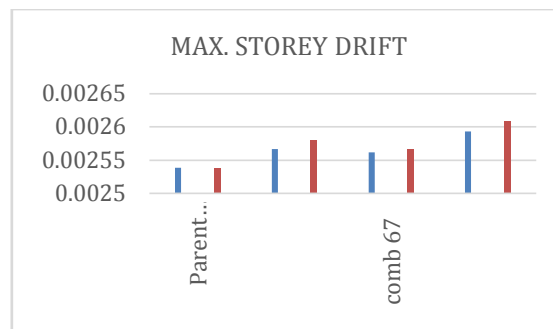


Fig-26: Maximum story displacement for case 11

Case 12 - Model having Mass & Stub column irregularity

Table 18: Maximum parameters for case 12

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 69 | EQx | 106.962454 | 0.002799 |
| | EQy | 108.196108 | 0.002772 |
| comb 70 | EQx | 107.314904 | 0.002584 |
| | EQy | 106.879519 | 0.00256 |
| comb 71 | EQx | 109.59702 | 0.002827 |
| | EQy | 109.866417 | 0.002798 |

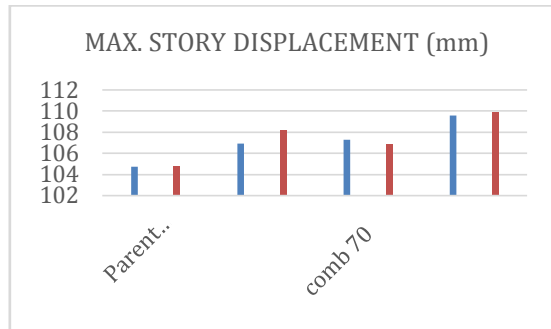


Fig-27: Maximum story displacement for case 12

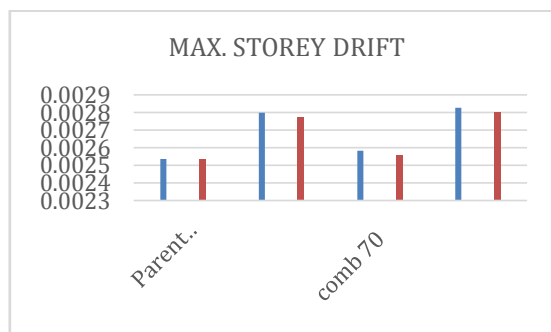


Fig-28: Maximum story displacement for case 12

Case 13 – Model having Vertical geometric & In-plane discontinuity irregularity

Table 19: Maximum parameters for case 13

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 72 | EQx | 114.304571 | 0.002779 |
| | EQy | 96.164031 | 0.002215 |
| comb 73 | EQx | 106.345721 | 0.002468 |
| | EQy | 106.625298 | 0.002473 |
| comb 74 | EQx | 113.436904 | 0.002768 |
| | EQy | 97.394031 | 0.002289 |
| comb 75 | EQx | 105.214692 | 0.002495 |
| | EQy | 105.153056 | 0.002485 |
| comb 76 | EQx | 81.356099 | 0.001899 |
| | EQy | 84.482978 | 0.001945 |
| comb 77 | EQx | 77.053739 | 0.001929 |
| | EQy | 76.911742 | 0.0019252 |
| comb 78 | EQx | 89.408658 | 0.002048 |
| | EQy | 88.200287 | 0.002037 |
| comb 79 | EQx | 79.744534 | 0.001757 |
| | EQy | 79.652071 | 0.001756 |
| comb 80 | EQx | 101.458061 | 0.00252 |

| | | | |
|---------|-----|------------|----------|
| | EQy | 105.140062 | 0.002609 |
| comb 81 | EQx | 103.539175 | 0.002629 |
| | EQy | 103.267757 | 0.002623 |

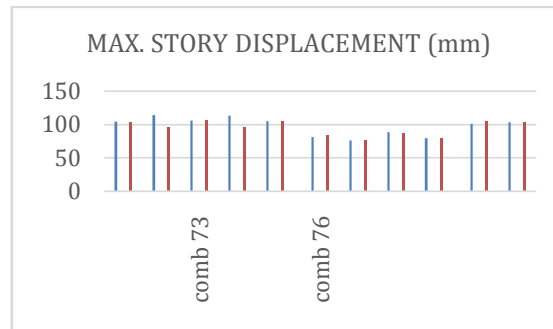


Fig-29: Maximum story displacement for case 13

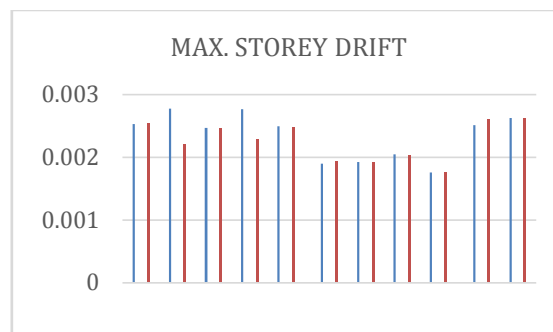


Fig-30: Maximum story displacement for case 13

Case 14 - Model having Vertical geometric & Stub column irregularity

Table 20: Maximum parameters for case 14

| MODEL | CASE | DISPLACEMENT (mm) | MAX. STORY DRIFT |
|---------|------|-------------------|------------------|
| Pa. Mo. | EQx | 104.74054 | 0.002538 |
| | EQy | 104.74054 | 0.002538 |
| comb 82 | EQx | 115.392668 | 0.003037 |
| | EQy | 96.976801 | 0.002315 |
| comb 83 | EQx | 107.168762 | 0.002641 |
| | EQy | 107.365592 | 0.002566 |
| comb 84 | EQx | 114.500873 | 0.00275 |
| | EQy | 98.117803 | 0.002282 |
| comb 85 | EQx | 106.19404 | 0.002479 |
| | EQy | 105.875879 | 0.002477 |
| comb 86 | EQx | 83.678341 | 0.00197 |
| | EQy | 85.618941 | 0.001967 |
| comb 87 | EQx | 79.400894 | 0.001967 |
| | EQy | 77.792751 | 0.001922 |
| comb 88 | EQx | 90.890204 | 0.00208 |

| | | | |
|---------|-----|------------|----------|
| | EQy | 89.741197 | 0.002075 |
| comb 89 | EQx | 81.211554 | 0.001872 |
| | EQy | 80.97665 | 0.00192 |
| comb 90 | EQx | 104.626167 | 0.002608 |
| | EQy | 107.045219 | 0.002637 |
| comb 91 | EQx | 106.971002 | 0.002676 |
| | EQy | 104.868721 | 0.00263 |

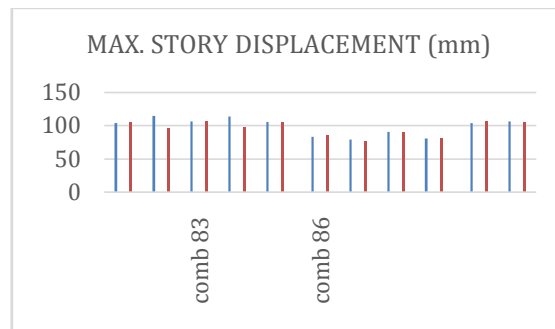


Fig-31: Maximum story displacement for case 14

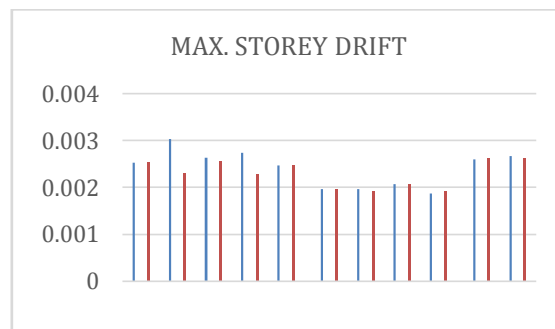


Fig-32: Maximum story displacement for case 14

VI. CONCLUSION

- [1]. Stiffness irregularities in the lower half of the building have a significant impact on the building's earthquake behaviour.
- [2]. Mass irregularity in the upper half of the building has a significant impact on the building's earthquake behaviour.
- [3]. If a building only has a setback on one side in either direction, vertical geometrical irregularity has a significant impact on its behaviour.
- [4]. In-plane discontinuity has an impact on the building's behaviour during an earthquake. If given in the bottom portion of the building.
- [5]. Stub column irregularity has an impact on the building's behaviour during an earthquake. If given in the lower half of the building.
- [6]. The stiffness irregularity is dominant nature over the mass irregularity.
- [7]. The participation of stiffness irregularity and vertical geometric irregularity is the same.
- [8]. Stiffness irregularity has a dominant nature over In-plane discontinuity.
- [9]. Stiffness irregularity has more impact than stub column irregularity.
- [10]. Vertical geometrical irregularity has a greater impact on structure behaviour than mass irregularity.
- [11]. Mass irregularity has a greater impact on structure behaviour than In-plane discontinuity.
- [12]. Stub column irregularity has a greater impact on building behaviour than mass irregularity.
- [13]. Vertical geometrical irregularity has a greater impact on building behaviour than In-plane discontinuity.
- [14]. Vertical geometrical irregularity has a greater impact on building behaviour than Stub column irregularity.

To begin with, the most serious irregularity is

Table 21: Most critical Vertical Irregularity

| Name of irregularity | % Change in Displacement | % Change in Drift |
|-----------------------------------|--------------------------|-------------------|
| Stiffness irregularity | 13.89 | 36.52 |
| Vertical geometrical irregularity | 8.26 | 8.79 |
| Stub column | 4.09 | 10.05 |
| Mass irregularity | 1.65 | 1.93 |
| In-plane discontinuity | 0.86 | 0.87 |

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